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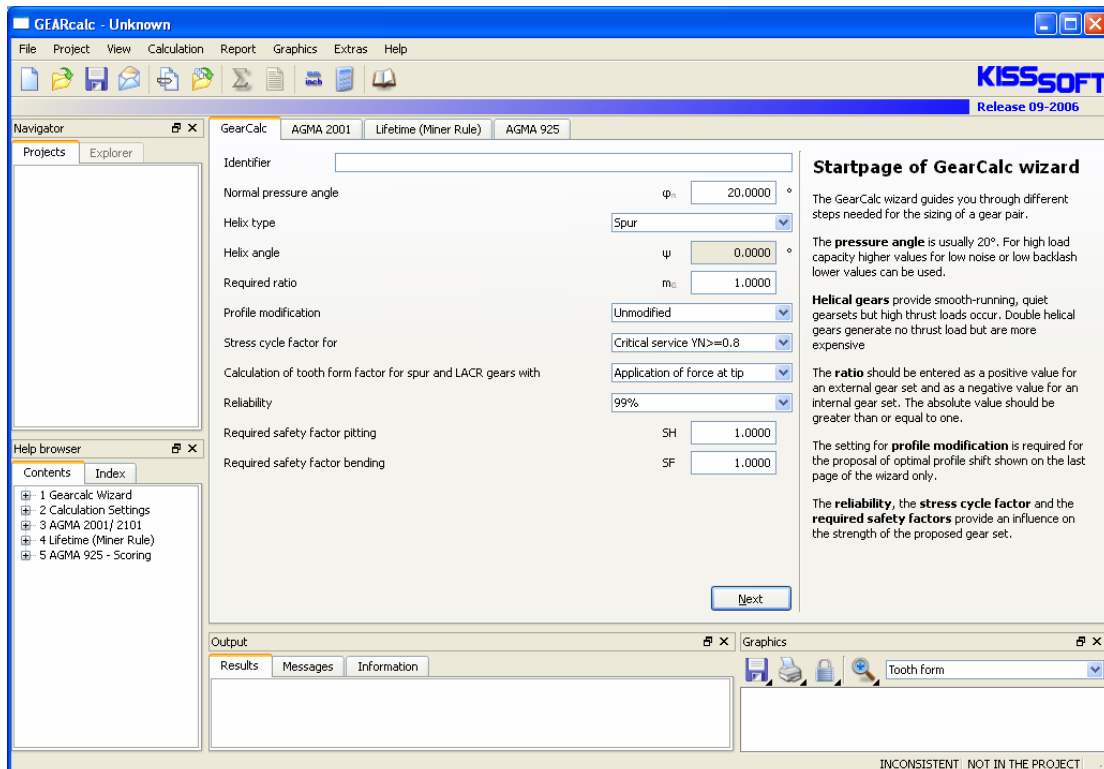
GEARCALC Tutorial 001: AGMA 2001

Keywords: AGMA 2001, GEARCALC
 For release:
 File: Dokument1
 Created / modified: 06.10.2006, M.Fish / 18.01.2007 A. Halter
 Download:

Starting GEARCALC

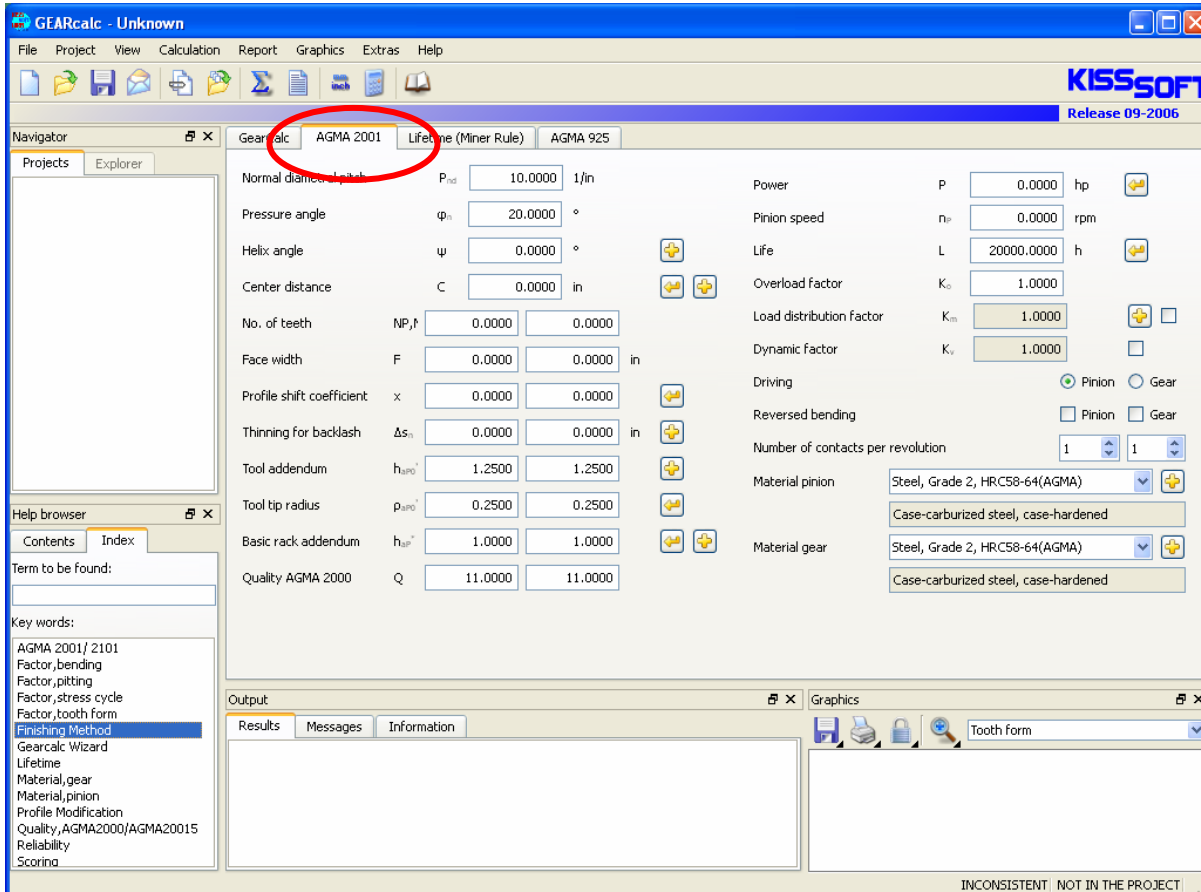
Starting GEARCALC

After installation, an icon can be found in the program list accessed using 'Start' in the bottom left hand corner of the screen. Alternatively click on the GEARCALC icon in the Windows Browser under "C:\Programs\GEARCALC\Bin\gearcalc.exe". The following window will appear:



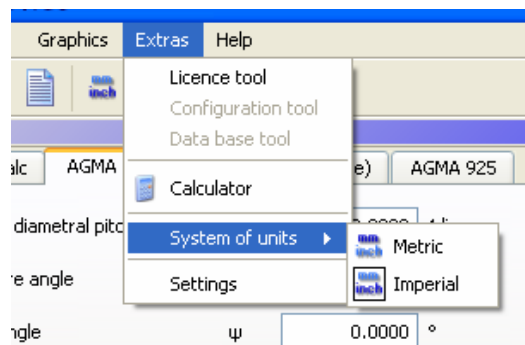
Select Calculation according to AGMA 2001

Click the tab AGMA 2001:



Selecting AGMA 2001 or AGMA 2101

If the program is set to use imperial units then the calculation will automatically be AGMA 2001. If this is changed to Newton units then the calculation method is AGMA 2101. To change the unit system select Extras > System of Units in the main menu.



Enter Data

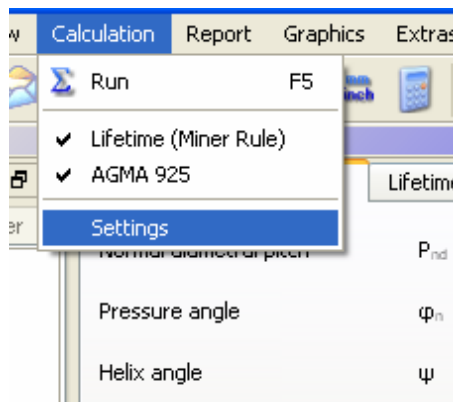
Task description – Motor 2:1 reduction set

A 60hp 1750rpm electric motor drives a belt conveyor through 2:1 reduction spur. This is a general industrial application and not critical in performance.

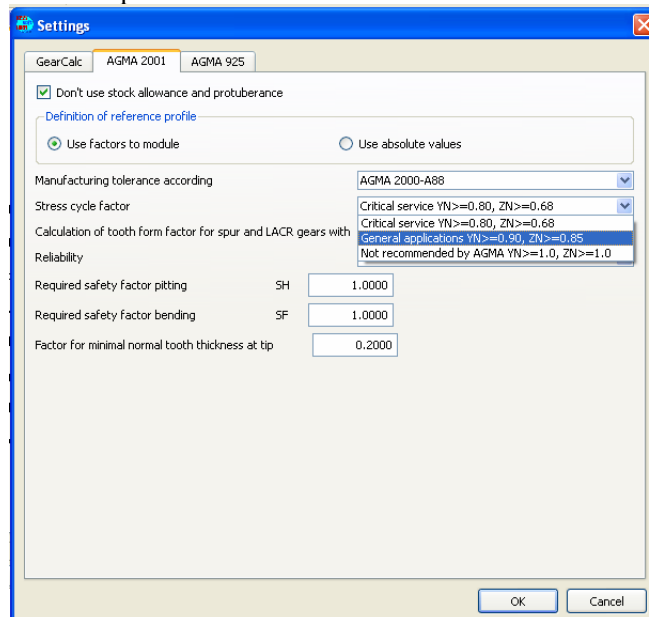
Enter Data For AGMA 2001

Define Operating Settings

Choose Calculation->Settings from the menu system:



A dialog containing the settings for the various settings will appear, and the AGMA 2001 tab will already be selected. The definition of the task calls for a calculation based on a general application. Set the “Stress cycle factor” to the “General applications” option as seen below:



Press OK to save the new settings and return to the main dialog.

Macro Geometry

The following geometry is defined for the example:

$$\begin{aligned}
 P_{nd} &= 10.0 \\
 \phi_C &= 20^\circ \\
 \psi_S &= 0^\circ \\
 C &= 3.75 \text{ in} \\
 N_S &= 25 \\
 N_G &= 50 \\
 F_1 &= 2 \text{ in} \\
 F_2 &= 2 \text{ in}
 \end{aligned}$$

$$x_1 = x_2 = 0.0$$

These values are entered directly in the cells provided:

The screenshot shows the GearCalc software interface with the following input values:

| Parameter | Value | Units |
|---------------------------|---------|-------|
| Normal diametral pitch | 10.0000 | 1/in |
| Pressure angle | 20.0000 | ° |
| Helix angle | 0.0000 | ° |
| Center distance | 3.75 | in |
| No. of teeth (Pinion) | 25 | |
| No. of teeth (Gear) | 50 | |
| Face width | 2.00 | in |
| Profile shift coefficient | 0.0000 | |

Tooth Thinning For Backlash

Both pinion and gear teeth are thinned 0.0024 in to obtain 0.0048 in backlash:

$$\Delta s_{n1} = \Delta s_{n2} = 0.0024 \text{ in}$$

Enter these values in both cells provided:

The screenshot shows the GearCalc software interface with the following input values for tooth thinning:

| Parameter | Value | Units |
|--------------------------------|--------|-------|
| Thinning for backlash (Pinion) | 0.0024 | in |
| Thinning for backlash (Gear) | 0.0024 | in |

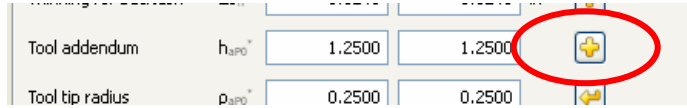
Tool Geometry

Tool Addendum

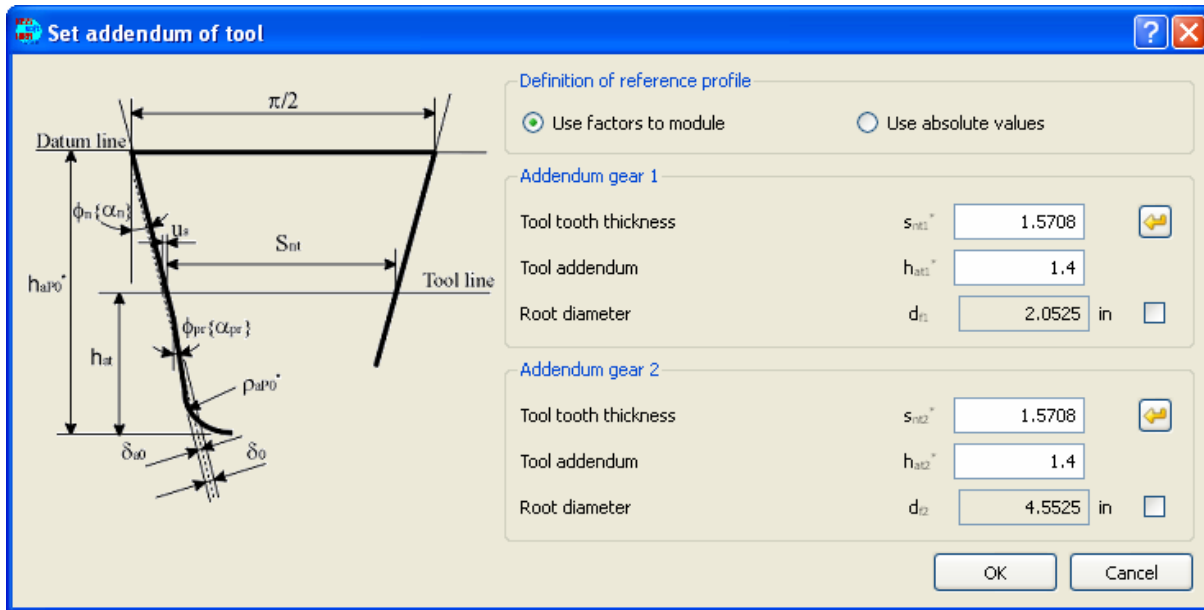
The gears are precision hobbled using the same hob. The definition of profile when set to 'Use factors to module' (in terms of $P_{nd} = 1.0$) is:

$$\begin{aligned}
 s_{nt}^* &= \pi/2 = 1.5708 \\
 h_{at}^* &= 1.4
 \end{aligned}$$

The plus button beside the 'Tool Addendum' field can be used to define the addendum form.



A window will open illustrating the profile definitions. Enter the values for s_{nt}^* and h_{at}^* in the cells for both gears. Click on the 'Root Diameter' cell after each value entry to ensure the correct value is recalculated.



Press OK to confirm the input and return to the main interface. The value of $h_{ap0}^* = 1.4$ is determined for both gears.

Tip Radius

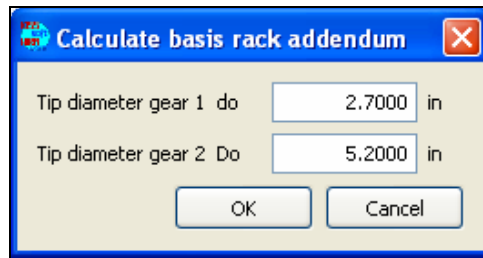
Enter the tip radius $\rho_{ap0}^* = 0.35$ for both gears in the cells provided.

Basic Rack Addendum

The tip diameter values d_0 and D_0 can be entered pressing the plus button beside the 'Basic Rack Addendum' field.



The following window will appear. In this case no adjustment will be needed, so simply confirm the existing values $d_0 = 2.7\text{in}$ and $D_0 = 5.2\text{in}$ by pressing OK.



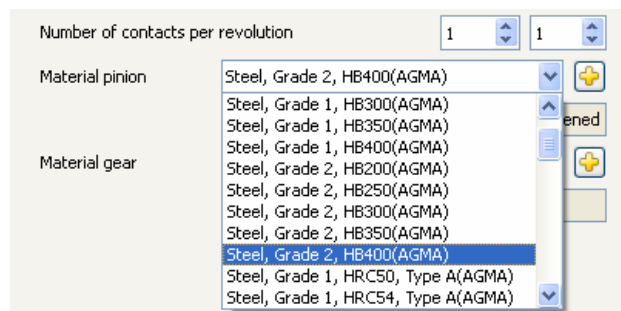
De-Rating Factors

Assume the transmitted power has been determined from field experience to be 60 hp. The pinion speed is 1750 rpm. Also assume the gear set is smooth running, evenly loaded and infrequently started/stopped. The overload factor is therefore set to unity. The load distribution factor, K_m , and dynamic factor, K_v , are left as unity and will be determined later by the calculation procedure for the given settings.

| | | | | |
|--------------------------|-------|------------|-----|--------------------------|
| Power | P | 60.0000 | hp | |
| Pinion speed | n_p | 1750.0000 | rpm | |
| Life | L | 20000.0000 | h | |
| Overload factor | K_o | 1.0000 | | |
| Load distribution factor | K_m | 1.0000 | | <input type="checkbox"/> |
| Dynamic factor | K_v | 1.0000 | | <input type="checkbox"/> |


Materials

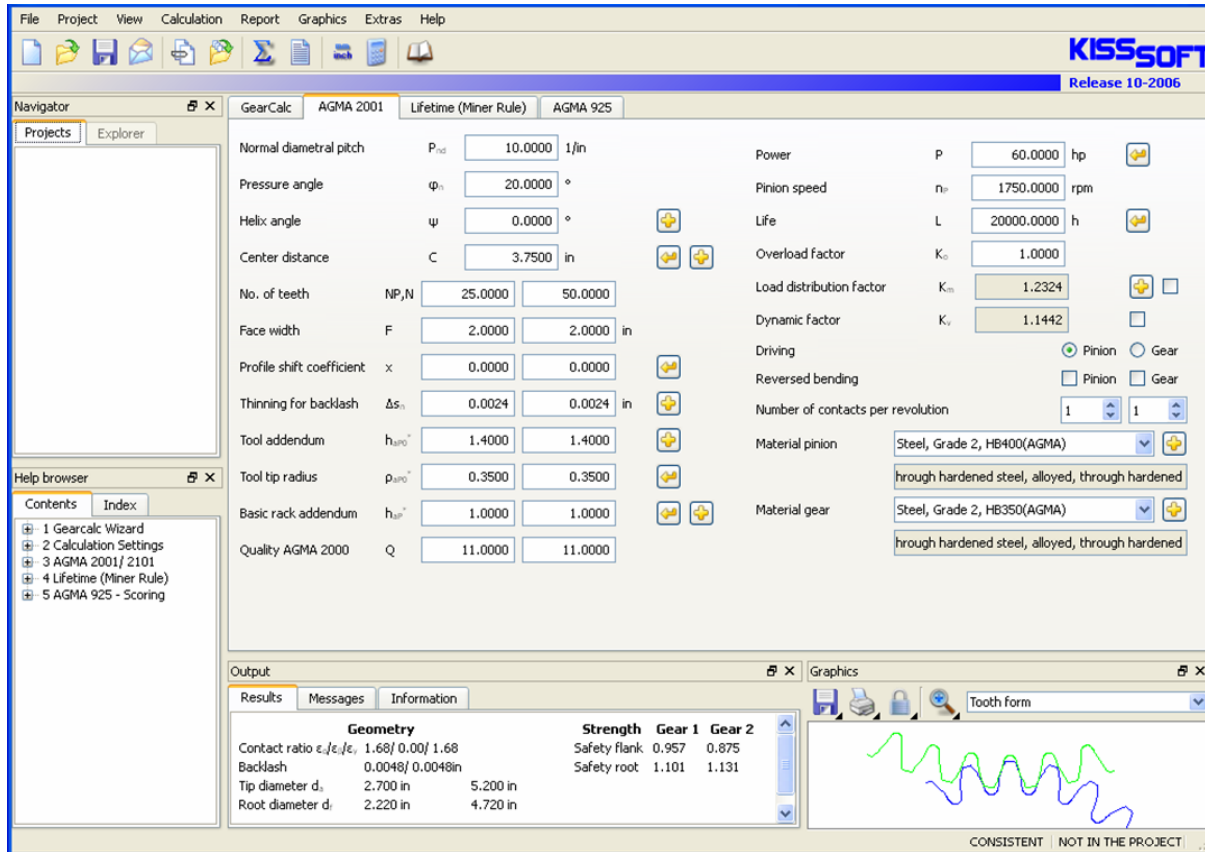
Choose the gear material 'Steel, Grade 2, HB400(AGMA)' from the drop down menu provided.



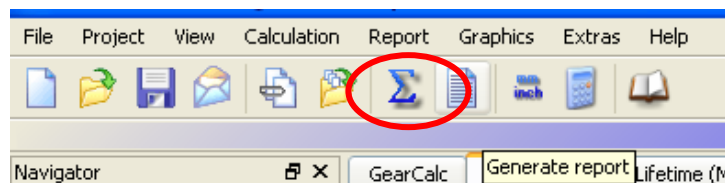
Repeat for the gear material but now select the 'Steel, Grade 2, HB350(AGMA)' entry.

Run Calculation after AGMA 2001 Data Entry

Run the AGMA 2001 calculation to check the data entry by clicking the calculate button: . On doing this, the tooth mesh and safety factors based on the input will be shown in the 'Graphics' and 'Output' windows respectively.



A text report is generated by pressing the 'Report' button in the toolbar above the interface:



A text report document for this analysis can be found in Annex I.

ANNEX I

KISSSOFT

Berechnungsprogramme für den Maschinenbau

GEARCALC - Release 10-2006

GEARCALC beta version

File

Name : Tutorial No 1 AGMA 2001

Changed by : MF on: 20.10.2006

at: 15:43:48

RESULTS FOR RESISTANCE CALCULATION FOLLOWING AGMA2001-D04 STANDARD

INPUT DATA SUMMARY

GEAR GEOMETRY DATA

| | | Pinion | Gear |
|-------------------------------|----------|-----------------|--------|
| Tooth number | NP,NG = | 25 | 50 |
| Net face width | F1,F2 = | 2.0000 | 2.0000 |
| Outside diameter | do,Do = | 2.7000 | 5.2000 |
| Normal diametral pitch (1/in) | Pnd = | 10.0000 | |
| Normal pressure angle | PHI(n) = | 20.0000 | |
| Standard helix angle | PSI(s) = | 0.0000 | |
| Operating center distance | C = | 3.7500 | |
| Centre distance tolerance | C.e/i = | 0.0000 / 0.0000 | |

Gear geometry data for Pnd = 1.0

| | | | |
|-------------------------------------|--------------------|---------|---------|
| Profile shift coefficient | X1,X2 = | 0.00000 | 0.00000 |
| Thinning for backlash | del.sn1, del.sn2 = | 0.02400 | 0.02400 |
| Stock allow. per side for finishing | Us1,Us2 = | 0.00000 | 0.00000 |

Tool geometry data for Pnd = 1.0

| | | | |
|-----------------------------|-----------------------|--------|--------|
| Tool normal tooth thickness | tce1,tce2 = | 1.5708 | 1.5708 |
| Tool addendum | haol,hao2 = | 1.4000 | 1.4000 |
| Tool tip radius | rTel,rTe2 = | 0.3500 | 0.3500 |
| Tool protuberance | DELTA(o1),DELTA(o2) = | 0.0000 | 0.0000 |

MATERIALS/HEAT-TREATMENT DATA

Material (Pinion) = Steel, Grade 2, HB400 (AGMA)
AGMA 2001-C95; AGMA 2101-C95

Material (Gear) = Steel, Grade 2, HB350 (AGMA)
AGMA 2001-C95; AGMA 2101-C95

Material type = Through hardened ste Through hardened ste

Heat-treatment = alloyed, through har alloyed, through har

LOAD DATA

| | | Pinion | Gear |
|---|--------|-----------|----------------------------|
| Transmitted power (HP) | P = | 60.0000 | |
| Pinion speed (rpm) | n(P) = | 1750.0000 | |
| Required life (HRS) | L = | 20000 | |
| Reliability | R = | 99 % | |
| Driving: | = | PINION | |
| Number of contacts per revolution | = | 1 | 1 |
| Reversed bending (0=No; 1=Yes) | = | 0 | 0 |
| Spur gear loading type | = | TIP | |
| Stress cycle factors, Curve chosen, Figs. 17 & 18 | = | Upper | (for general applications) |

DERATING FACTORS

| | | | |
|----------------------------------|------|--------|--------|
| Overload (or application) factor | Ko = | 1.0000 | |
| Size factor | Ks = | 1.0000 | |
| Surface condition factor | Cf = | 1.0000 | |
| Rim thickness factor | KB = | 1.0000 | 1.0000 |

| | | |
|--------------------------|------|--------|
| Load distribution factor | Km = | 1.2324 |
| Dynamic factor | Kv = | 1.1442 |

GEOMETRY SUMMARY-1

| | | Pinion | Gear |
|------------------------------|----------|---------------|---------------|
| Generating pitch dia | ds, Ds = | 2.5000 | 5.0000 |
| Operating pitch dia | d, D = | 2.5000 | 5.0000 |
| Base dia | db, Db = | 2.3492 | 4.6985 |
| Mean dia of pinion | dm = | 2.5000 | |
| Root diameter (manufactured) | dR, DR = | 2.2134/2.2134 | 4.7134/4.7134 |
| Limit (SAP) (manufactured) | dc, Dc = | 2.3733 | 4.8579 |
| Top of fillet (manufactured) | de, De = | 2.3541/2.3541 | 4.8051/4.8051 |

PRESSURE ANGLES

| | | |
|----------------------|-----------|---------|
| Standard transverse | PHI (s) = | 20.0000 |
| Operating transverse | PHI (t) = | 20.0000 |
| Standard normal | PHI (c) = | 20.0000 |
| Operating normal | PHI (n) = | 20.0000 |

HELIX ANGLES

| | | |
|-----------|-----------|--------|
| Standard | PSI (s) = | 0.0000 |
| Operating | PSI = | 0.0000 |
| Base | PSI (b) = | 0.0000 |

PITCHES

| | | |
|----------------------|------|---------|
| Transverse diametral | Pd = | 10.0000 |
| Transverse circular | p = | 0.3142 |
| Normal circular | pn = | 0.3142 |
| Transverse base | pb = | 0.2952 |
| Normal base | pN = | 0.2952 |
| Axial | px = | ----- |

DISTANCES ALONG LINE OF ACTION

| | | |
|---------------------------------------|------|--------|
| Start of active profile (SAP) | C1 = | 0.1685 |
| Low single tooth contact (LPSTC) | C2 = | 0.3702 |
| Pitch point | C3 = | 0.4275 |
| High single tooth contact (HPSTC) | C4 = | 0.4637 |
| End of active profile (EAP) | C5 = | 0.6654 |
| Distance between interference points | C6 = | 1.2826 |
| Active length of line of action | Z = | 0.4969 |
| Pinion addendum portion of Z | Za = | 0.2379 |
| Pinion dedendum portion of Z | Zb = | 0.2590 |
| Dist. from pitch point to stress calc | Zc = | 0.0573 |

LENGTH OF CONTACT LINE

| | | |
|---------|--------|--------|
| Minimum | Lmin = | 2.0000 |
| Maximum | Lmax = | 4.0000 |
| Average | Lavg = | 3.0000 |

RATIOS

| | | |
|------------------------------|------|--------|
| Contact length | mL = | 2.0000 |
| Transverse (profile) contact | mp = | 1.6832 |
| Axial (face) contact | mF = | 0.0000 |
| Total contact | mt = | 1.6832 |
| Gear ratio | mG = | 2.0000 |
| Load sharing (mN = F/Lmin) | mN = | 1.0000 |

TRANSVERSE RADII OF CURVATURE

| | | |
|------------------------------------|------|--------|
| At operating pitch point of pinion | RP = | 0.4275 |
| At operating pitch point of gear | RG = | 0.8551 |
| At point of stress calc of pinion | R1 = | 0.3702 |
| At point of stress calc of gear | R2 = | 0.9124 |

TOOTH DEPTHS

| | | | |
|---------------------|------------|--------|--------|
| Operating addendum | a1, a2 = | 0.1000 | 0.1000 |
| Operating dedendum | b1, b2 = | 0.1433 | 0.1433 |
| Operating clearance | c1, c2 = | 0.0433 | 0.0433 |
| Whole depth | ht1, ht2 = | 0.2433 | 0.2433 |
| Working depth | hK = | 0.2000 | |

TRANSVERSE CIRCULAR TOOTH THICKNESSES (manufactured)

| | | | |
|------------|-----------|---------------|---------------|
| Topland | to1,to2 = | 0.0694/0.0694 | 0.0750/0.0750 |
| Operating | tr1,tr2 = | 0.1547/0.1547 | 0.1547/0.1547 |
| Generating | tg1,tg2 = | 0.1547/0.1547 | 0.1547/0.1547 |
| Base | tb1,tb2 = | 0.1804/0.1804 | 0.2154/0.2154 |

NORMAL CIRCULAR TOOTH THICKNESSES (manufactured)

| | | | |
|------------|-------------|---------------|---------------|
| Topland | tno1,tno2 = | 0.0694/0.0694 | 0.0750/0.0750 |
| Operating | tnr1,tnr2 = | 0.1547/0.1547 | 0.1547/0.1547 |
| Generating | tnl1,tnl2 = | 0.1547/0.1547 | 0.1547/0.1547 |
| Base | tnb1,tnb2 = | 0.1804/0.1804 | 0.2154/0.2154 |

| | | | |
|-------------|---------|--------|--------|
| LEAD | L1,L2 = | 0.0000 | 0.0000 |
|-------------|---------|--------|--------|

OPERATING CIRCULAR BACKLASH (manufactured)

| | |
|---|----------------|
| Transverse (only through Center dist. tol.) = | 0.0000/ 0.0000 |
| Transverse (total) B = | 0.0048/ 0.0048 |
| Normal (total) Bn = | 0.0045/ 0.0045 |

PROFILE SHIFT COEFFICIENTS FOR MANUFACTURING

| | | | |
|--------------------------|-----------|------------------|------------------|
| Theoretical, no backlash | X1,X2 = | 0.0000 | 0.0000 |
| Manufacturing | Xe1,Xe2 = | -0.0330/ -0.0330 | -0.0330/ -0.0330 |

NOTE: All dims in inches, all angles in degrees.
 All geometry data, which are not declared as 'manufacturing',
 are for the theoretical (no backlash) tooth meshing situation.

GEOMETRY SUMMARY-2**PITTING RESISTANCE GEOMETRY FACTOR DATA**

| | | |
|------------------------------------|-----------|--------|
| Helical overlap factor | C (PSI) = | 1.0000 |
| Minimum length of contact | Lmin = | 2.0000 |
| Pitting resistance geometry factor | I = | 0.0990 |

BENDING STRENGTH GEOMETRY FACTOR DATA

| | | Pinion | Gear |
|---|-----------|---------------|-------------|
| Load angle | PHI (L) = | 28.059 | 24.544 |
| Height of Lewis parabola | h = | 1.8902 | 1.9199 |
| Tooth thickness at critical section | t = | 1.8683 | 2.0914 |
| Radius at curvature of fillet curve | ro = | 0.4365 | 0.3952 |
| Loaded at tip (No load sharing) (h, t, ro for Pnd = 1.0) | | | |
| Diameter of the critical point F | DFpoint = | 2.2958 | 4.7866 |
| Helical factor | Ch = | 1.0000 | |
| Helix angle factor | K (PSI) = | 1.0000 | |
| Stress correction factor | Kf = | 1.4172 | 1.5143 |
| Tooth form factor | Y = | 0.3593 | 0.4277 |
| Bending strength geometry factor | J = | 0.2535 | 0.2824 |

LOAD / MATERIAL SUMMARY

| | | |
|---|--------|--------|
| Pitch line velocity (FPM) | vt = | 1145.4 |
| Transmitted tangential load (LB.) | Wt = | 1728.7 |
| Torque transmitted by pinion (LB.IN.) | T(1) = | 2160.9 |
| Torque transmitted by gear (LB.IN.) | T(2) = | 4321.7 |
| Contact load factor for pitting resist. | K = | 518.4 |
| Unit load factor for bending strength | U(L) = | 8640.5 |

MATERIALS/HEAT TREATMENT DATA

| | | | |
|---|--------------------|----------|----------|
| Modulus of elasticity (lb/in ²) | EP,EG = | 30000000 | 30000000 |
| Poisson's ratio | MU (P),MU (G) = | 0.3000 | 0.3000 |
| Surface hardness | HB 400 | HB 350 | |
| Allowable contact stress | SAC (P), SAC (G) = | 173900 | 156450 |
| Allowable bending stress | SAT (P), SAT (G) = | 57200 | 52100 |

DERATING FACTOR SUMMARY

| | | | |
|------------------------------------|------------------|--------|--------|
| Overload (or application) factor | Ko = | 1.0000 | |
| Size factor | Ks = | 1.0000 | |
| Surface condition factor | Cf = | 1.0000 | |
| Rim thickness factor | KB = | 1.0000 | 1.0000 |
| Load distribution factor | Km = | 1.2324 | |
| Transmission accuracy grade number | Qnu = | 10 | |
| Dynamic factor | Kv = | 1.1442 | |
| Combined derating factor pitting | Ko*Kv*Km*Ks*Cf = | 1.4101 | |
| Combined derating factor bending | Ko*Kv*Km*Ks*KB = | 1.4101 | |

Km CALCULATED USING AGMA2001/2101 METHOD (CHAPTER 15)

Gear unit type: Commercial enclosed gear unit

| | | |
|---|-------|--------|
| Mesh alignment factor | Cma = | 0.1582 |
| Mounting procedure: Without contact improvement at assembly | | |
| Mesh alignment correction factor | Ce = | 1.0000 |
| Gearing: Without longitudinale flank correction | | |
| Lead correction factor | Cmc = | 1.0000 |
| Pinion proportion factor | Cpf = | 0.0675 |
| Pinion proportion modifier | Cpm = | 1.1000 |
| Large offset pinion (s1/s >= 0.175) | | |
| Face load distribution factor | Cmf = | 1.2324 |

NOTE: Transverse load distribution factor Cmt = 1.0

STRENGTH SUMMARY

| | | Pinion | Gear |
|---|--------|---------------|-------------|
| Stress cycle factor (Contact) | Z(N) = | 0.8843*a* | 0.8985*a* |
| Surface condition factor | C(f) = | 1.0000 | 1.0000 |
| Hardness ratio factor | C(H) = | 1.0000 | 1.0000 |
| Temperature factor | K(T) = | 1.0000 | 1.0000 |
| Reliability factor | K(R) = | 1.0000 | |
| Allow. contact stress No. (lb/in ²) | Sac = | 153779 | 140571 |
| Stress cycle factor (Root) | Y(N) = | 0.9253*a* | 0.9367*a* |
| Reverse loading factor | = | 1.0000 | 1.0000 |
| Allow. bending stress No. (lb/in ²) | Sat = | 52924 | 48804 |

a NOTE: Based on life (HRS) L = 20000
Curve chosen, Figs. 17 & 18 = Upper (for general applications)

STRESS SUMMARY

| | | |
|---|-------|----------|
| Elastic coefficient (lb ^{.5} /in) | Cp = | 2290.0 |
| Contact stress No. (lb/in ²) | Sc = | 160726.5 |
| Pinion bending stress No. (lb/in ²) | St1 = | 48058.8 |
| Gear bending stress No. (lb/in ²) | St2 = | 43139.0 |

RESULTING SAFETY FACTORS

| | | | |
|-------------------------|----------|------|------|
| Safety factor (Bending) | Sat/st = | 1.10 | 1.13 |
| Safety factor (Contact) | Sac/sc = | 0.96 | 0.87 |

SERVICE FACTORS

| | | | |
|-----------------------------|-------|------|------|
| Service factor for bending | KSF = | 1.10 | 1.13 |
| Service factor for contact | CSF = | 0.92 | 0.76 |
| Service factor for gear set | SF = | 0.76 | |

POWER RATING CALCULATION

(Calculation of the transmittable power)

| | | Pinion | Gear *a* |
|---|--------|---------------|-----------------|
| Allow. transmitted power for pitting (HP) | Pac = | 54.92 | 45.90 |
| Allow. transmitted power for bending (HP) | Pat = | 66.07 | 67.88 |
| Allowable transmitted power (HP) | P = | 45.90 | |
| Life factor for pitting resistance | Z(N) = | 0.884 *b* | 0.899 *b* |
| Life factor for bending resistance | Y(N) = | 0.925 *b* | 0.937 *b* |
| Durability (Pitting) life (HRS) | L(C) = | 20000.0 | 20000.0 |
| Durability (Pitting) life (CYCS/10^6) | N(C) = | 2100.0 | 1050.0 |
| Bending fatigue life (HRS) | L(T) = | 20000.0 | 20000.0 |
| Bending fatigue life (CYCS/10^6) | N(T) = | 2100.0 | 1050.0 |

a NOTE: Based on allowable stresses at life (HRS) L = 20000

b NOTE: Pitting and Bending Life calculated for general applications
(Upper portion in fig. 17 and 18)

MANUFACTURING DATA

Tooth thickness dimensions

| | | Pinion | Gear |
|-------------------------------------|-------|----------------|--------------------|
| Thinning for backlash | As = | 0.0024/ 0.0024 | 0.0024/ 0.0024 |
| Normal circular tooth thickness | sn = | 0.1547/ 0.1547 | 0.1547/ 0.1547 |
| Span measurement | Wk = | 0.7708/ 0.7708 | 1.6914/ 1.6914 |
| Number of teeth spanned | k = | 3.0000 | 6.0000 |
| Diameter of span contact point | dWk = | 2.4724 | 4.9936 |
| Measurement over 1 ball | MrK = | 1.3673/ 1.3673 | 2.6184/ 2.6184 |
| Measurement over 2 balls | MdK = | 2.7295/ 2.7295 | 5.2369/ 5.2369 *c* |
| Ball or roll diameter | DM = | 0.1728 | 0.1728 |
| Diameter of ball/roll contact point | dMM = | 2.4979 | 5.0022 |
| Normal chordal thickness | 'sn = | 0.1546/ 0.1546 | 0.1547/ 0.1547 *a* |
| Normal chordal height | ha = | 0.1025 | 0.1012 |

a NOTE: Tooth thickness measured at generating pitch diameter

c NOTE: When measuring over 2 balls, the two balls must be in the same transverse plane.

NOTE: All dims in inches.

Tolerances

Following AGMA 2000-A88:

| | | | |
|---|--------------|------|------|
| Accuracy grade | Q-AGMA2000 = | 11 | 11 |
| Pitch Variation Allowable (mil) | VpA = | 2.6 | 2.9 |
| Runout Radial Tolerance (mil) | VrT = | 8.7 | 10.2 |
| Profile Tolerance (mil) | VphiT = | 3.3 | 3.7 |
| Tooth Alignment Tolerance (mil) | VpsiT = | 4.3 | 4.3 |
| Composite Tolerance, Tooth-to-Tooth (mil) | VqT = | 5.5 | 5.5 |
| Composite Tolerance, Total (mil) | VcqT = | 14.2 | 15.7 |

NOTE: All dims in 1/10000 in.

End report

lines: 330